

Effect of some factors on the electrolysis production of sodium perchlorate from sodium chlorate using PbO₂/Pb-Ti electrode

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ABSTRACT

The electrolysis process of sodium perchlorate production from sodium chlorate using PbO₂/Pb-Ti electrode was studied by linear sweep voltammetry (LSV), electrochemical impedance spectroscopy (EIS) and electrolysis efficiency evaluation. The results showed that the technological parameters (sodium chlorate concentration, temperature, electrolyte current density, additive content and pH) strongly affected the polarization, charge transfer resistance and electrolysis efficiency. Therefore, the appropriate technological mode for the electrolysis process was selected as: NaClO₃ concentration 300 - 600 g/L; temperature 50 °C; current density 0.15 - 0.2 A/cm²; NaF additive concentration 1-2 g/L; solution pH 7.

Keywords: Sodium perchlorate; Electrolysis; Sodium chlorate; PbO₂ electrode.

1. INTRODUCTION

Sodium perchlorate (NaClO₄) is considered the most important compound among perchlorates [1] because it is a precursor for the manufacture of main components (NH₄ClO₄, LiClO₄, KClO₄) in explosives, solid fuels, pyrotechnics, fireworks and other compounds. The safe and economical method for manufacturing NaClO₄ is electrolytic oxidation of sodium chlorate (NaClO₃) followed by crystallization. In which the positive electrode and electrolysis conditions (concentration of reactants, electrolysis current density, solution pH, temperature, type and content of additives) play an important role in the oxidation capacity of NaClO₃, electrolysis efficiency, power consumption, and product purity during the electrolysis process. Generally, the efficiency of the electrochemical process depends on the initial concentration of the raw materials [2, 3]. In most cases, high concentrations of reactants are used to avoid mass transfer limitations. Higher current densities can increase the rate of perchlorate production, but excessive current can lead to electrode degradation or side reactions. Elevated temperatures are often used to improve reaction kinetics, however, the temperature needs to be controlled to avoid unwanted side reactions. Maintaining a slightly acidic pH (e.g., below 9) is often preferred for efficient perchlorate formation. Some additives, such as sodium dichromate (for Pt anodes) and sodium fluoride (for lead dioxide anodes), are also used to improve the electrolysis performance [2, 4]. The choice of electrode material is crucial, as different materials have varying overpotentials for the desired reactions. Common types of positive electrodes that have been studied and used are magnetite, mixed metal oxide, graphite, diamond, Pt, PbO₂ [2-10]. The PbO₂ electrode shows the advantages of low oxidation potential of NaClO₃, high cumulative efficiency (50 - 70%), stability and cost savings [11-14]. This electrode is usually fabricated through a complex and costly process by chemically coating PbO₂ on a titanium or carbon substrate. This paper proposes a simple electrochemically produced titanium-based PbO₂ electrode and studies the influence of some technological factors on the electrolysis process of NaClO₄ production on this electrode.

2. EXPERIMENT

2.1. Materials and chemicals

Chemicals NaClO₃, NaOH, Pb(NO₃)₂, H₃BO₃, HNO₃, HF, NaF, Na₂SO₄ are chemicals used for analysis (Origin: China).

2.2. Prepare PbO₂/Pb-Ti electrode

The working electrodes for electrochemical measurements and the positive electrode (anode) for the electrolytic cell are made from titanium plates with active surface areas after finishing of 1 cm² and 200 cm² respectively, through the following stages: (i) Cutting the electrode blanks from 1 mm thick flat titanium plates; (ii) Degreasing in alkaline solution, activating in a mixed solution of HNO₃ and HF, and plating 50^{±3} μm thick lead (measured by micrometer) in a fluoroborate solution; (iii) Electrolysis to create a stable brown PbO₂ film in 20% Na₂SO₄ solution with a current density of 1 A/dm², temperature 25 °C, time 3 hours [15]; (iv) The inactive surface parts of the electrodes are sealed with epoxy glue.

The counter electrode in electrochemical measurements and the negative electrode in the electrolytic cell were made from SUS 304 stretched mesh, measuring 100 × 100 × 1.5 (mm).

2.3. Electrochemical measurements

Electrochemical measurements were carried out on a Zennium Pro apparatus (Zahner – Germany) using a three-electrode system. The working electrode and the counter electrode were a PbO₂/Pb-Ti electrode and SUS 304 expanded mesh, respectively, fabricated as in section 2.2. The reference electrode was an Ag/AgCl electrode.

Polarization measurements were carried out at a linear potential sweep rate of 1 mV/s, ranging from the equilibrium electrode potential to +2 V (Ag/AgCl) in electrolyte solutions with compositions and temperatures as shown in table 1.

Electrochemical impedance measurements were carried out at equilibrium potential, amplitude of 5 mV, frequency range from 10 kHz to 50 mHz in electrolyte solutions with compositions and temperatures as shown in table 1.

2.4. Evaluation of electrolysis efficiency

To evaluate the effect of technological parameters on electrolysis efficiency, electrolysis was carried out with a PbO₂/Pb-Ti anode electrode and a SUS 304 cathode plate fabricated as described in section 2.2. The solution composition and electrolysis mode to evaluate each parameter are specified in section 2.5. The electrode assembly and electrolysis cell are shown in figure 1, in which the volume of the studied electrolysis solution is 2 liters.

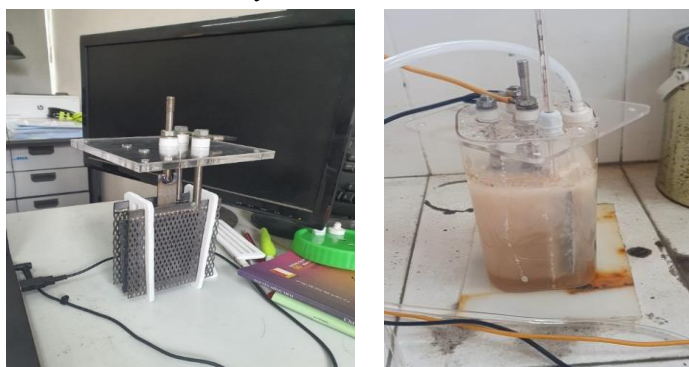


Figure 1. Electrode pair and test electrolytic cell.

The electrolysis efficiency of producing NaClO₄ from NaClO₃ is calculated using the following formula:

$$H(\%) = \frac{m_{tt}}{m_{it}} = \frac{(C_0 - C_f) \times V \times n \times F}{A \times i \times S \times 3600 \times t} \times 100\% \quad (1)$$

Here: H (%) is the efficiency of NaClO₃ electrolysis current; C₀ (g/L) and C_f (g/L) are the initial and final NaClO₃ concentrations (determined by ion liquid chromatography according to TCVN

6494-4 : 2000) of the electrolysis solution, respectively; V (L) is the volume of the electrolysis cell, $V = 2$ liters; n is the number of electrons exchanged, $n = 2$; F is the Faraday constant, 96500 C/mol; A is the molar mass of NaClO_3 , $A = 106.44$ g/mol; i (A/cm^2) is the electrolysis current density; S (cm^2) is the area of the $\text{PbO}_2/\text{Pb-Ti}$ electrode, $S = 200$ cm^2 and t (hours) is the electrolysis time.

2.5. Study on the influence of some technological parameters

The effects of some technological parameters, including initial concentration of NaClO_3 (C_0 – g/L), temperature, anode current density, C_{NaF} additive concentration and solution pH on the electrolysis process were studied by evaluating the current efficiency in the corresponding solution components and electrolysis modes as shown in table 1; combined with electrochemical measurement methods in the corresponding solutions.

Table 1. Solution composition and electrolysis mode for the study.

Technology parameters	Electrolyte solution composition			Electrolysis technology mode		
	C_0 (g/l)	C_{NaF} (g/L)	pH	i_A (A/cm^2)	Time (hours)	Temperature ($^\circ\text{C}$)
Initial concentration of NaClO_3	750	0	7	-	-	30
	600	0	7	0.15	6	30
	450	0	7	-	-	30
	300	0	7	0.15	4	30
	150	0	7	0.15	4	30
Temperature	600	0	7	0.15	6	30
	600	0	7	0.15	6	50
	600	0	7	0.15	6	70
Electrolytic current density	600	0	7	0.05	18	50
	600	0	7	0.10	9	50
	600	0	7	0.15	6	50
	600	0	7	0.20	4.5	50
	600	0	7	0.25	3.6	50
Additive content	600	0	7	0.15	6	50
	600	1	7	0.15	6	50
	600	2	7	0.15	6	50
	600	2	7	0.15	13	50
pH	600	2	5	0.15	13	50
	600	2	7	0.15	13	50
	600	2	9	0.15	13	50

3. RESULTS AND DISCUSSION

3.1. Effect of concentration NaClO_3

Figure 2 shows the anodic polarization curves of the $\text{PbO}_2/\text{Pb-Ti}$ electrode in the range from the equilibrium potential E_0 to + 2.0 V (Ag/AgCl) at 30 $^\circ\text{C}$ in a solution with a NaClO_3 concentration of 150 – 750 g/L. It can be seen that as the NaClO_3 concentration increases in the solution from 150 to 450 g/L, the polarization curve shifts toward a more negative potential. This is the result of a decrease in concentration polarization due to an increase in the concentration of the reactant. However, as the NaClO_3 concentration continues to increase from 450 to 750 g/L, the polarization curve shifts toward a more positive potential. This result is because when the NaClO_3 concentration in the solution increases (exceeding 450 g/L), the diffusion of the reaction product (NaClO_4) from the electrode surface into the solution becomes more difficult. From figure 2, it can also be inferred that, in the electrolysis process of producing NaClO_4 from NaClO_3 on $\text{PbO}_2/\text{Pb-Ti}$

electrode, the electrolysis process should start and end at the initial and final concentrations of NaClO_3 of 600 g/L and 300 g/L, respectively, to ensure energy saving.

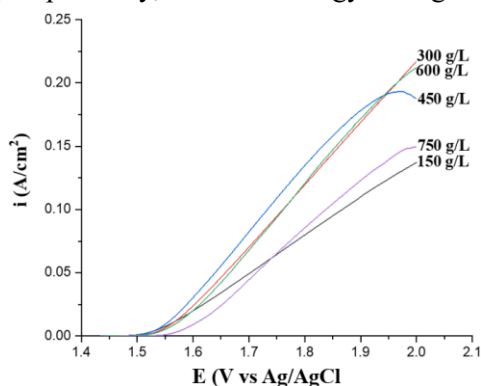


Figure 2. Anode polarization curve on $\text{PbO}_2/\text{Pb-Ti}$ electrode in the potential range from E_0 to +2.0 V (Ag/AgCl) at 30 °C in a solution with a NaClO_3 concentration of 150 – 750 g/L.

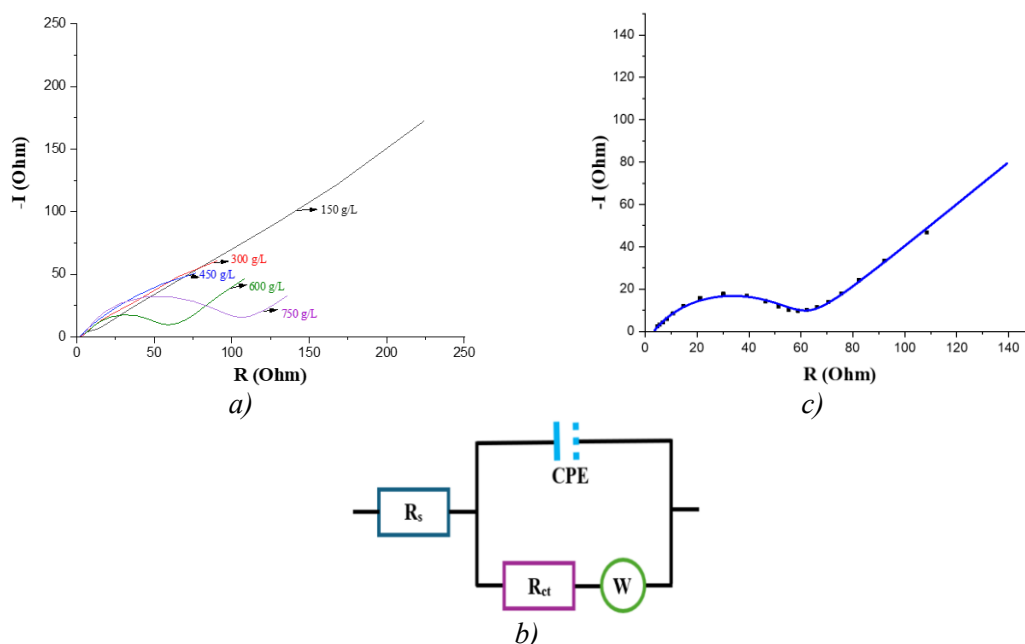


Figure 3. Electrochemical impedance spectra of $\text{PbO}_2/\text{Pb-Ti}$ electrode at equilibrium potential in electrolyte solutions with NaClO_3 concentrations from 150 g/L to 750 g/L (a); equivalent electrochemical circuit (b) and simulated impedance spectrum of the equivalent circuit with the impedance spectrum measured at NaClO_3 concentration of 600 g/L (c).

Figure 3a shows the electrochemical impedance spectrum of the $\text{PbO}_2/\text{Pb-Ti}$ electrode at the equilibrium potential E_0 , temperature 30 °C, potential amplitude 5 mV, frequency range from 10 kHz to 30 mHz, in a solution with NaClO_3 concentration from 150 – 750 g/L. Figure 3b is the equivalent circuit used to simulate the electrochemical process occurring on the $\text{PbO}_2/\text{Pb-Ti}$ electrode. In which R_s (Ω) is the resistive element, representing the solution resistance. CPE is the constant phase element, representing the capacitance of the electric double layer, R_{ct} (Ω) is the resistive element, representing the charge transfer resistance. W is the Warburg impedance, representing the diffusion layer impedance. Figure 3c shows the simulated impedance curve (solid line) obtained by fitting the equivalent circuit of figure 3b to the actual impedance curve measured at a NaClO_3 concentration of 600 g/L (discontinuous square dotted line).

The simulated impedance spectrum is relatively similar to the measured impedance curve with a fitting error of 4.9%, showing that the equivalent circuit in figure 3b simulates well the electrochemical process occurring on the PbO₂/Pb-Ti electrode. The electrochemical parameters obtained from fitting the equivalent circuit to the impedance spectrum in figure 3a are shown in table 2. In the measurement, C_{dl} (μF) is the double-layer capacitance and σ_w is the Warburg coefficient. It can be seen that the resistance of the electrolyte solution reaches its minimum value at a NaClO₃ concentration of 600 g/L. The charge transfer resistance gradually decreases when the NaClO₃ concentration increases to 450 g/L and then gradually increases when the reactant concentration continues to increase. The variation of the Warburg coefficient shows that the NaClO₃ concentration of 450 g/L is the most favorable for the diffusion of reactants and reaction products into/out of the electrode surface.

Table 2. Effect of NaClO₃ concentration on electrochemical parameters.

Concentration of NaClO ₃ (g/L)	Electrochemical parameters			
	R _s (Ω)	R _{ct} (Ω)	C _{dl} (μF)	σ _w (DW)
150	1.425	73.89	26.9	413.9
300	1.332	3.041	20.9	78.82
450	1.329	1.108	0.278	40.22
600	1.313	57.88	14.99	48.11
750	1.367	103.2	29.36	79.08

Table 3 shows the change in current efficiency when electrolysis is carried out at 30 °C, anode current density of 0.15 A/cm², pH 7, with initial NaClO₃ concentrations in the solution of 150, 300, 600 g/L, respectively. It can be seen that the efficiency of the electrolysis process gradually decreases as the electrolysis concentration range of NaClO₃ decreases. In particular, at the low concentration range (starting at 150 g/L and ending at 45.5 g/L), the efficiency of the electrolysis process decreases sharply to only 43.9%.

Table 3. Effect of NaClO₃ concentration on electrolysis efficiency.

No.	Initial concentration of NaClO ₃ , g/l	Final concentration of NaClO ₃ , g/l	Electrolysis efficiency, %
1	600	326	76,7
2	300	151	68,2
3	150	45,5	43,9

3.2. Effect of temperature on electrolysis

Figure 4 is the impedance spectra on the PbO₂/Pb-Ti electrode obtained in an electrolyte solution with a NaClO₃ concentration of 600 g/L at an equilibrium electrode potential, a potential amplitude of 5 mV, a frequency range from 10 kHz to 30 mHz, with temperatures of 30, 50 and 70 °C. The electrochemical parameters obtained by fitting the measured results to the equivalent circuit of figure 3b are shown in table 4. It is found that at 50 °C, the electrolysis process has the smallest charge transfer resistance and diffusion resistance.

Table 5 shows the change in current efficiency when electrolysis is carried out at an anode current density of 0.3 A/cm², time of 6 hours, pH 7, initial NaClO₃ concentration in the solution of 600 g/L, with temperatures of 30, 50 and 70 °C, respectively. It is found that, when the electrolysis temperature increases, the current efficiency decreases. This can be explained by the fact that increasing the electrolysis temperature makes the oxygen escape process more favorable. However, increasing the solution temperature to 50 °C will reduce the power consumption due to the reduction of solution resistance, charge transfer resistance and diffusion resistance (as seen in table 4) without much decrease in electrolysis efficiency (-4.2%). Therefore, the temperature of 50 °C is suitable for the electrolysis process.

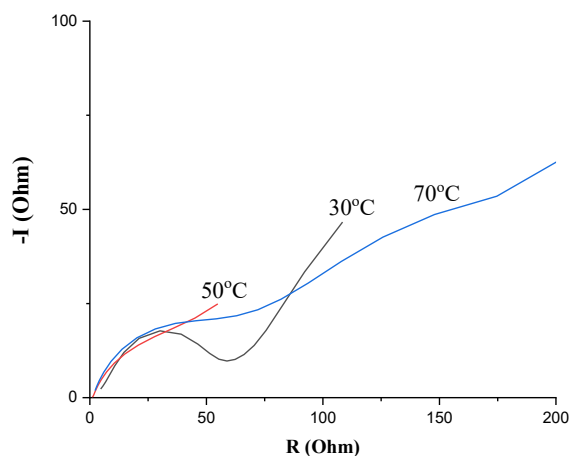


Figure 4. Electrochemical impedance spectra of $PbO_2/Pb-Ti$ electrode at equilibrium potential at different electrolyte solution temperatures.

Table 4. Effect of electrolysis temperature on electrochemical parameters.

Temperature (°C)	Electrochemical parameters			
	R_s (Ω)	R_{ct} (Ω)	C_{dl} (μF)	σ_w (DW)
30	1.313	57.88	14.99	28.11
50	1.073	56.12	12.9	9.663
70	1.065	89.16	15.33	54.61

Table 5. Effect of temperature on electrolysis efficiency.

No.	Initial concentration of $NaClO_3$, g/l	Final concentration of $NaClO_3$, g/l	Temperature, °C	Electrolysis efficiency, %
1	600	326	30	76.7
2	600	341	50	72.5
3	600	354	70	68.8

3.3. Effect of electrolysis current density

Table 6 shows the change in current efficiency when electrolysis is carried out in a solution with an initial concentration of $NaClO_3$ of 600 g/L, temperature of 50 °C, solution pH of 7, with current densities of 0.05, 0.1, 0.15, 0.2 and 0.25 A/cm^2 , respectively. As the electrolysis current density increases, the electrolysis efficiency increases. However, in the current density range from 0.15 to 0.2 A/cm^2 , when the current density increases, the efficiency does not increase much. Even when the current density increases to 0.25 A/cm^2 , the electrolysis efficiency decreases slightly. This is explained by the fact that the electrolysis process of producing $NaClO_4$ from $NaClO_3$ is always accompanied by a side reaction of releasing oxygen. When the electrolysis current density increases, the proportion of current devoted to the oxidation of $NaClO_3$ increases, leading to an increase in electrolysis efficiency. However, due to the limitation of reactant concentration and diffusion limit, when increasing the electrolysis current density beyond a certain value, the partial current for $NaClO_3$ oxidation does not increase. At that time, increasing the current density only increases the current ratio of the oxygen gas release process, leading to a decrease in electrolysis efficiency. On the other hand, when electrolysis occurs at high current density, the gas release process occurs strongly, increasing the risk of destroying the porous electrode. From the above results, it can be seen that the appropriate electrolysis current density for $NaClO_3$ electrolysis is 0.15 - 0.2 A/cm^2 .

Table 6. Effect of current density on electrolysis efficiency.

No.	Initial concentration of NaClO ₃ , g/l	Final concentration of NaClO ₃ , g/l	Current density, (A/cm ²)	Electrolysis efficiency, %
1	600	394	0.05	57.6
2	600	360	0.10	67.2
3	600	341	0.15	72.5
4	600	338	0.20	73.3
5	600	339	0.25	73.0

3.4. Effects of additives

Table 7 shows the change in current efficiency when electrolysis is carried out at an anode current density of 0.15 A/cm², pH 7, initial NaClO₃ concentration of 600 g/L, temperature of 50 °C, in solutions without and with 1 and 2 g/L of NaF additive, respectively. It is found that the presence of NaF additive with concentrations of 1 and 2 g/L increases the electrolysis efficiency by 1.1 and 5.6%, respectively. In particular, with a NaF additive concentration of 2 g/L, the electrolysis efficiency is still maintained at 71.7% even when electrolysis is performed in the low NaClO₃ concentration range (down to 45 g/L). The effect of increasing the electrolysis efficiency of NaF can be explained by the adsorption of F⁻ ions on the electrode surface, increasing the oxygen release potential and thus improving the current fraction for NaClO₃ oxidation. The ability to maintain high electrolysis efficiency of PbO₂/Pb-Ti electrode with NaF additive at low concentration of reactant shows similarity with other types of PbO₂ electrodes [7] that have been studied and manufactured. This shows the prospect of applying this electrode to a practical electrolysis process.

Table 7. Effect of additives on electrolysis efficiency.

No.	Initial concentration of NaClO ₃ , g/l	Final concentration of NaClO ₃ , g/l	Additive concentration NaF, g/l	Electrolysis efficiency, %
1	600	341	0	72.5
2	600	317	1	73.6
3	600	321	2	78.1
4	600	45	2	71.7

3.5. Effect of pH on electrolysis

Table 8 shows the change in current efficiency when electrolysis was carried out at an anode current density of 0.15 A/cm², time of 6 hours, initial NaClO₃ concentration in solution of 600 g/L, temperature of 50 °C, NaF concentration of 2 g/L, with solution pH of 5, 7 and 9, respectively. It can be seen that the current efficiency was highest at the neutral level and decreased further at the alkaline level. On the other hand, when electrolysis was performed at a pH of 9, the solution became cloudy with suspended yellow-brown solids, possibly due to anode corrosion. Therefore, pH 7 was chosen for the electrolysis process.

Table 8. Effect of solution pH on electrolysis efficiency.

No.	Initial concentration of NaClO ₃ , g/l	Final concentration of NaClO ₃ , g/l	pH	Electrolysis efficiency, %
1	600	65	5	69.1
2	600	45	7	71.7
3	600	91	9	65.7

4. CONCLUSIONS

Depending on the results of this study, the following conclusions can be drawn:

i) Technological factors (concentration of reactants, electrolysis current density, temperature, solution pH and additives) strongly affect the kinetic parameters as well as the efficiency of the electrolysis process to produce sodium perchlorate from sodium chlorate on PbO₂/Pb-Ti electrode. The appropriate electrolysis conditions obtained are: NaClO₃ concentration 300 – 600 g/L; temperature 50 °C; electrolysis current density 0.15 – 0.2 A/cm²; NaF concentration 2 g/L; pH 7.

ii) PbO₂/Pb-Ti electrodes fabricated by the electrochemical method are promising for application in the practical electrolysis process of producing NaClO₄.

REFERENCES

- [1]. T. Chongcheng, Y. Pei, “Method for producing sodium perchlorate”, Patent CN 1012742B, (1991).
- [2]. Henry C. Miller, John C Grigger, “Method of producing perchlorates”, Patent US2813825A, (1957).
- [3]. Javier Llanos et al., “Electrochemical production of perchlorate as an alternative for the valorization of brines”, Chemosphere, Vol. 220, pp. 637-643 (2019).
- [4]. Ahmed D. Wiheeb, “The manufacture of perchlorate by direct method using graphite substrate lead dioxide (Gsd) anode”, Diyala Journal of Engineering Sciences, Vol. 2(1), pp. 66-79 (2009).
- [5]. Jean-Christophe Millet, Michel Jaccaud, “Continuous electrolytic production of alkali metal perchlorates”, Patent US 5004527, (1991).
- [6]. Handady V. K. Udupa et al., “Electrolytic preparation of perchlorate”, Patent US3493478, (1970).
- [7]. M. Cheraghveisi et al., “Electrosynthesis of perchlorate using neodymium-doped PbO₂ electrode: application of experimental design methodology for optimization of the effective parameters”, Materials Research Express, Vol. 9(2), pp. 1-10 (2022).
- [8]. Sai Bhavaraju, James Steppan, “Bismuth metal oxide pyrochlores as electrode materials”, Patent EP 2443269A2, (2012).
- [9]. A. Sánchez-Carretero et al., “Electrochemical production of perchlorates using conductive diamond electrolyses”, Chemical Engineering Journal, Vol. 166(2), pp. 710-714, (2011).
- [10]. L. J. J. Janssen, P. D. L. Van Der Heyden, “Mechanism of anodic oxidation of chlorate to perchlorate on platinum electrodes, Journal of Applied Electrochemistry”, Vol. 25 (2), pp. 126 – 136, (1995).
- [11]. Takashi Osuga, Shojiro Fujii, Kiichiro Sugino, Taro Sekine, “Electrolytic production of perchlorate by lead dioxide anodes”, Journal of The Electrochemical Society, Vol. 116 (2), pp. 203 -207, (1969).
- [12]. Joseph C. Schumacher et al., “Electrolytic production of Sodium perchlorate using Lead dioxide anodes”, Journal of The Electrochemical Society, Vol. 105 (3), pp. 151, (1958).
- [13]. Rossano Amadelli, A. B. Velichenko, “Lead dioxide electrodes for high potential anodic processes”, Journal of the Serbian Chemical Society, Vol. 66 (11-12), pp. 835-845 (2001).
- [14]. M. Munichandraiah et al., “Kinetics and mechanism of anodic oxidation of chlorate ion to perchlorate ion on lead dioxide electrodes”, Journal of Applied Electrochemistry, Vol. 17, pp. 33-48, (1987).
- [15]. Z. Chen et al., “A novel Pb/PbO₂ electrodes prepared by the method of thermal oxidation-electrochemical oxidation: Characteristic and electrocatalytic oxidation performance”, Journal of Alloys and Compounds, Vol. 851, pp. 156834, (2021).

TÓM TẮT

Ảnh hưởng của một số yếu tố tới quá trình điện phân chế tạo natri perchlorate từ natri chlorat sử dụng điện cực PbO₂/Pb-Ti

Quá trình điện phân chế tạo natri perchlorate từ natri chlorate sử dụng điện cực PbO₂/Pb-Ti đã được nghiên cứu bằng phương pháp quét thế tuyến tính (LSV), phổ tổng trở điện hóa (EIS) và đánh giá hiệu suất điện phân. Kết quả cho thấy các thông số công nghệ (nồng độ natri chlorate, nhiệt độ, mật độ dòng điện phân, hàm lượng phụ gia và pH) ảnh hưởng mạnh đến sự phân cực, điện trở chuyển điện tích và hiệu suất điện phân. Từ đó, chế độ công nghệ thích hợp cho quá trình điện phân được lựa chọn là: nồng độ NaClO₃ 300 – 600 g/L; nhiệt độ 50 °C; mật độ dòng điện 0,15 - 0,2 A/cm²; nồng độ phụ gia NaF 1-2 g/L; pH dung dịch 7.

Từ khóa: Natri perchlorate; Điện phân; Natri chlorate; Điện cực PbO₂.